



Vincenzo Paolo Loschiavo

Tutor: Prof. Eng. Raffaele Albanese
XXIX Cycle – I year presentation

**Addressing the power exhaust
in the next generation fusion reactor**

Background

WHY?????

- Discover the secrets of the thermonuclear fusion
- Improve knowledge and skills

To



From
Mechanical
Engineering

Question: is it so strange????

Answer: well...probably not!

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2 thesis carried out (bachelor and M.Sc. degree) on the thermonuclear fusion

Background

%Research Group Topic:

- Tokamak Divertor Definition and Design
(Prof. Raffaele Albanese is the Project Leader for
DTT II facility - Divertor Test Tokamak)

%Fellowship:

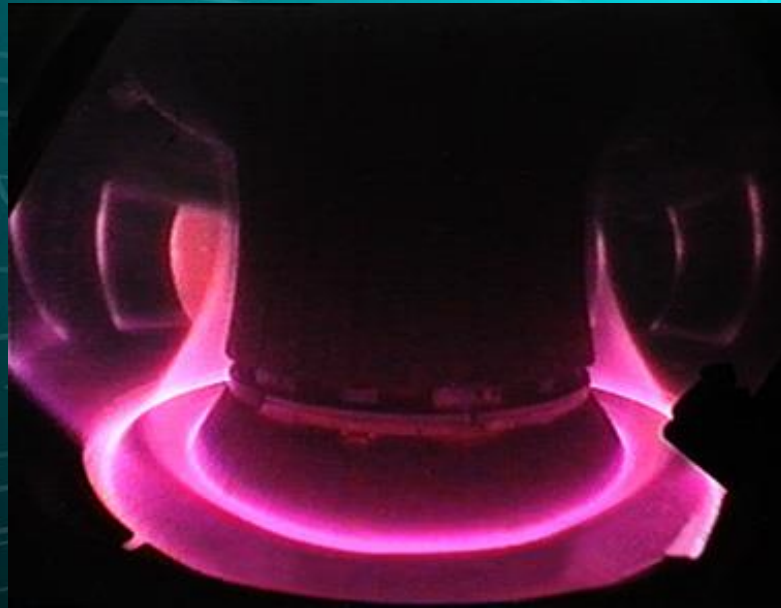
- PhD supported by grant

%Cooperations:

- EUROfusion (Garching - Max Planck Institut fur
plasma physics)
- ENEA (Brasimone - Frascati)
- ...and many more!

My problem

**“Addressing the power exhaust
in the next generation fusion reactor”**



Find the best way to spread the huge heat load -POWER EXHAUST- (up to transient 30 MW/m²) impinging on the material surfaces in a next generation fusion reactor.

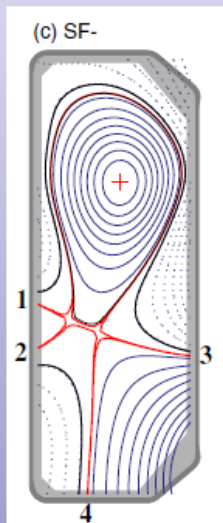
My problem

- State of the art (possible solutions)

1) Advanced divertors

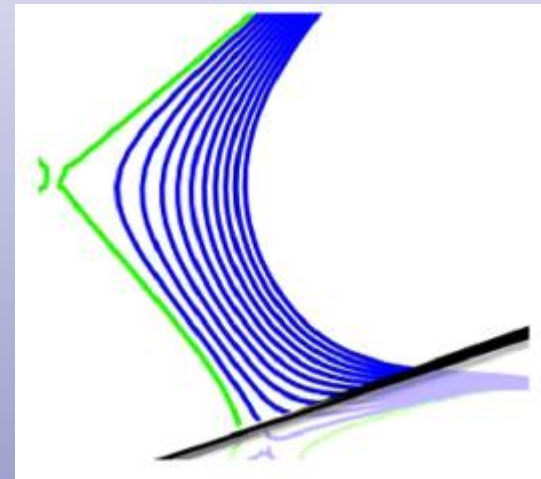
Snowflake

$$d_{xpt} \rightarrow 0$$
$$0 \leq \theta_{xpt} \leq \pi/2$$



X-Divertor

$$d_{xpt} \cong d_s$$
$$\theta_{xpt} \cong \theta_s$$



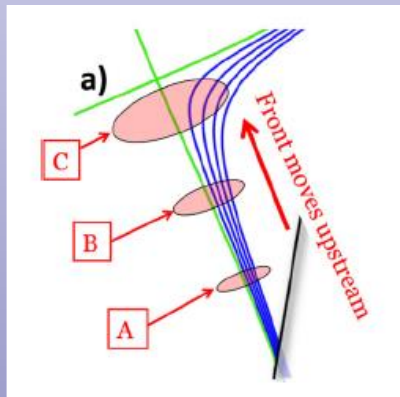
My problem

- State of the art (possible solutions)

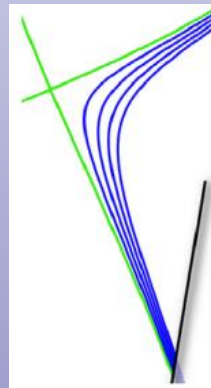
2) Plasma Detachment

The Snowflake ($DI < 1$) The Standard Divertor ($DI = 1$) The X-Divertor ($DI > 1$)

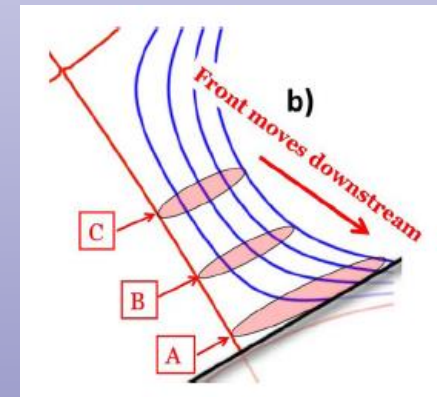
The Snowflake Divertor ACCELERATES the movement of the detachment front towards the main X-point.



Reference



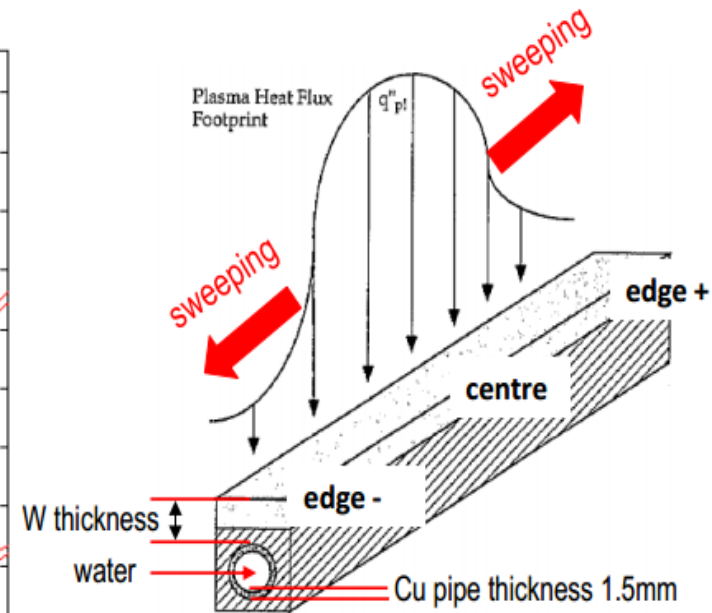
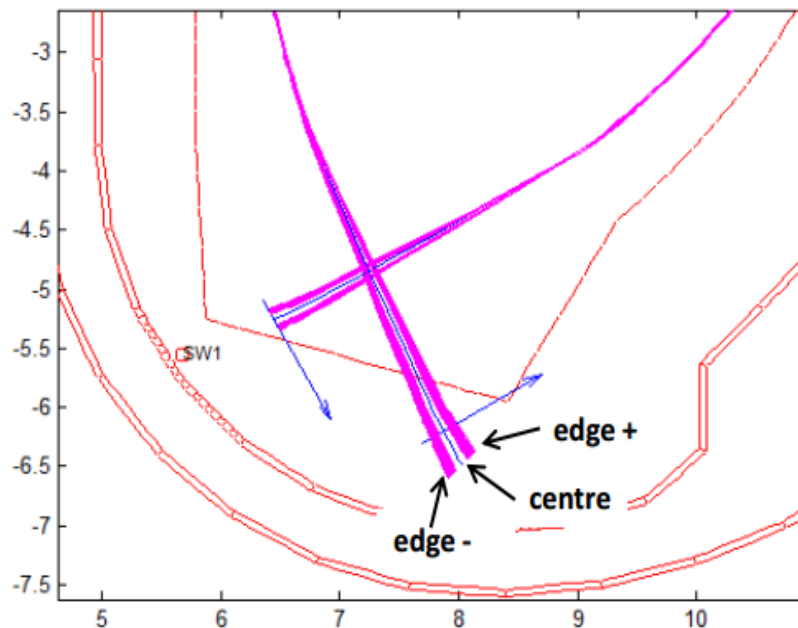
The X-Divertor RETARDS the movement of the detachment front towards the main X-point.



My problem

The strike point sweeping
a periodical movement of the strike points

sweeping: periodic strike points oscillation



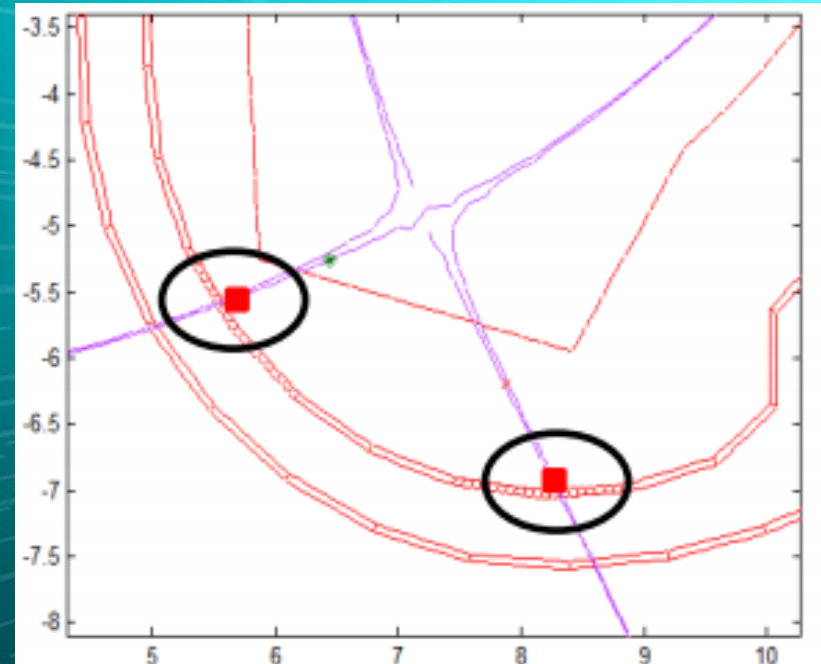
My problem

The strike point sweeping
a periodical movement of the strike points

The strike point sweeping is produced by dedicated in-vessel coils connected in antiserie

The power needed for sweeping in the above conditions (240 kAt amplitude, 120 kAt rms) is:

- active power of 0.30 MW at 0.2 Hz, 3.3 MW at 1 Hz
- reactive power of 3.5 MVar at 0.2 Hz, 16 MW at 1 Hz



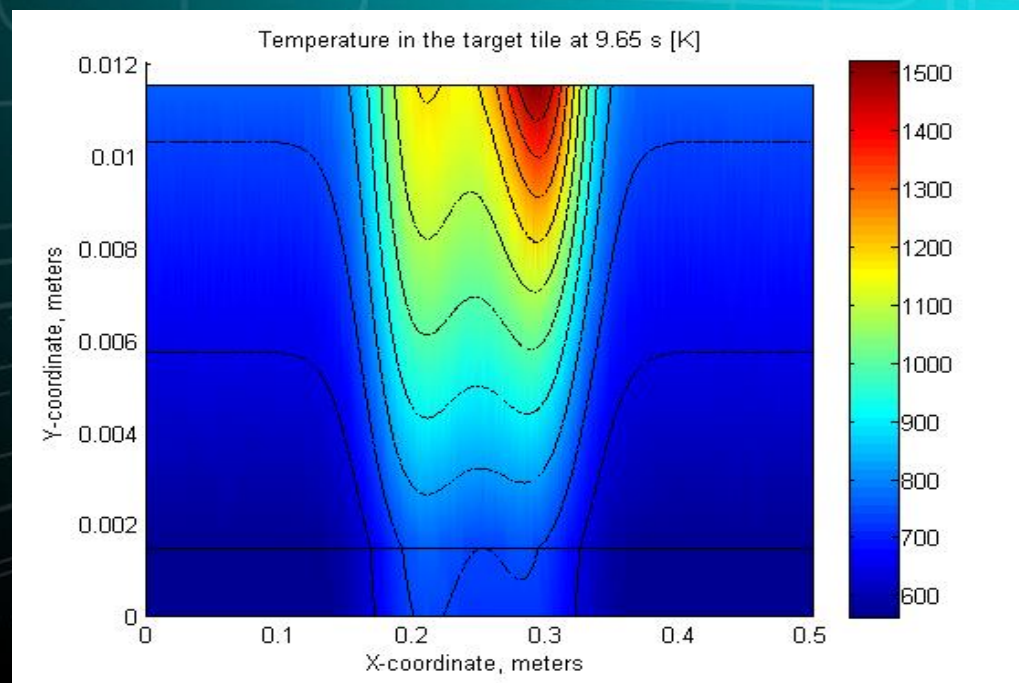
My research activity

Idea

Investigate the strike points sweeping effect on the material surfaces temperature reduction

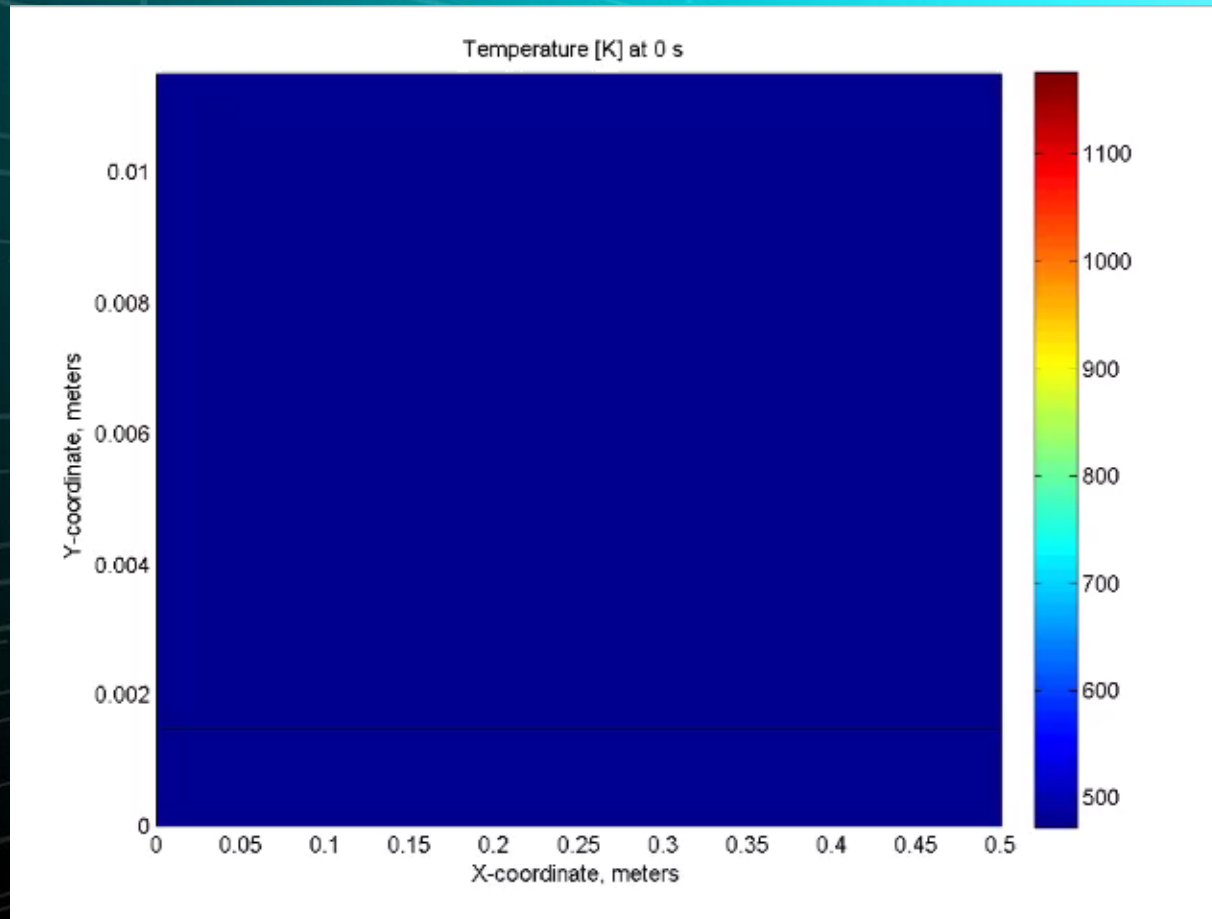
Methodology:

2-D FEM model implementation (my main contribution)



My research activity

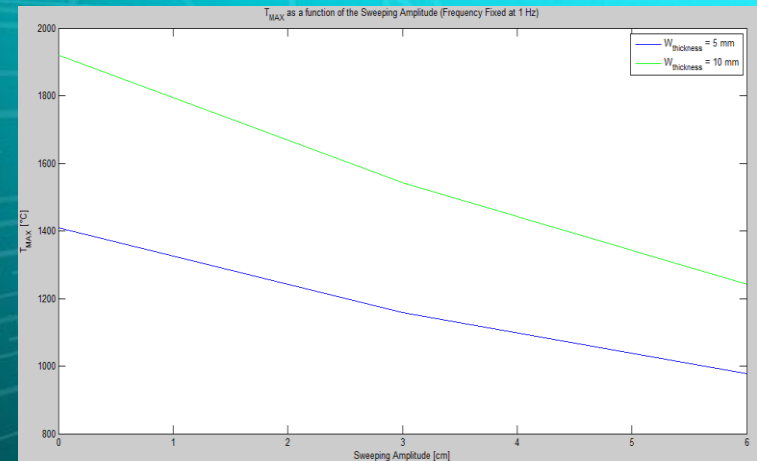
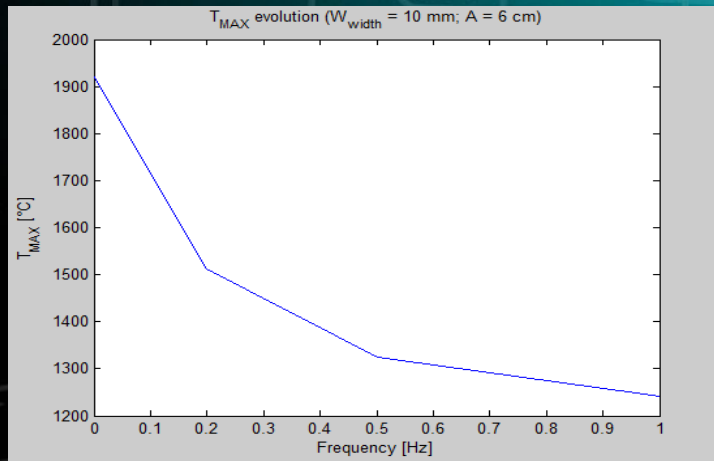
Effectuated results



My research activity

Effected results

- sensitivity analysis of the material surfaces temperature reduction depending on the main sweeping parameters (amplitude and frequency)



$f \uparrow \Rightarrow T \downarrow$

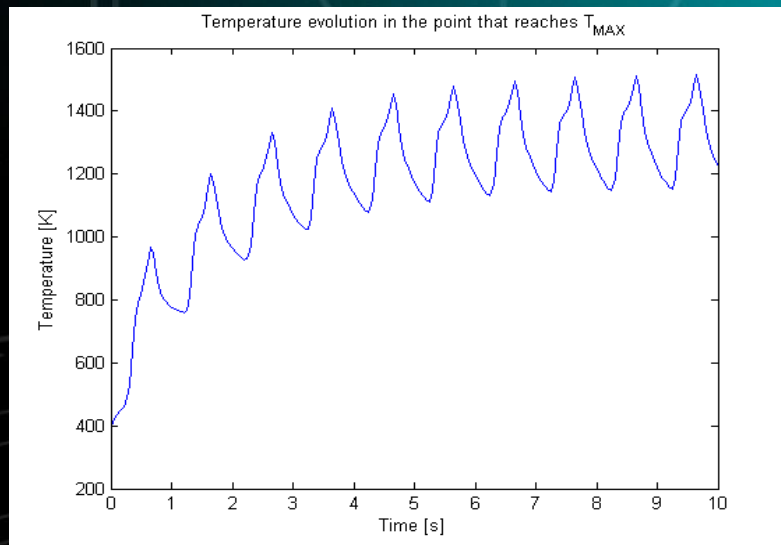
amplitude $\uparrow \Rightarrow T \downarrow$

My research activity

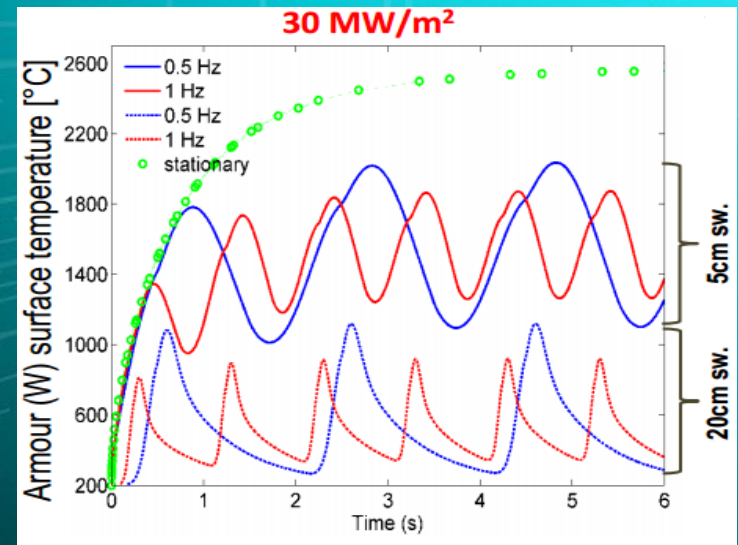
Validation

comparisons with other 1-D and 3-D models

2-D model



3-D model



My research activity

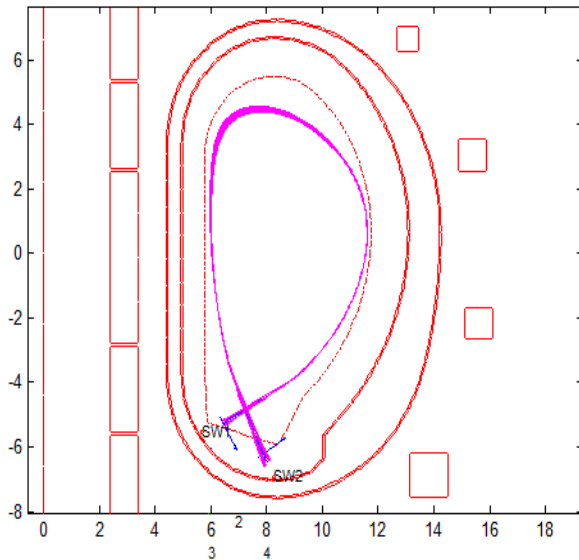
Developments

This 2-D model is just the starting point for implementing a 3-D FEM model in order to quantify and whenever possible reduce the effects of:

- the thermal fatigue on the plasma facing components.

Taking into account:

- the AC losses due to the dB/dt on the superconducting coils;
- the motion of the plasma core;
- neutron shielding.



My products

One workshop paper

F. Maviglia

with contribution from:

G. Federici, G. Strohmayer, R. Wenninger, C. Bachmann, R.
Albanese, R.

Ambrosino, M. Li, V.P. Loschiavo et al.

“Limitations of transient power
loads on DEMO divertor and
analysis of mitigation
techniques”

Presented at the EFPW, 1 - 3 December 2014, Split, Croatia

My First year credits

	Credits year 1							Summary
	Estimated	1	2	3	4	5	6	
	bimonth	bimonth	bimonth	bimonth	bimonth	bimonth	bimonth	
Modules	21			3		3	5	11
Seminars	5	0,4	0,8		1	0,2	2	4,4
Research	34	10	8	8	8	6	3	43
	60	10	8,8	11	9	9,2	10	58

Courses I attended during the first year:

- PLASMAS AND CONTROLLED THERMONUCLEAR FUSION (Section A);
- NUMERICAL METHODS FOR ENGINEERS;
- INTRODUCTION TO QUANTUM MECHANICS;
- EUROPEAN PROJECTS;
- RESEARCH PROJECT MANAGEMENT.

My First year credits

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Seminars	5	0,4	0,8		1	0,2	2	4,4
Research	34	10	8	8	8	6	3	43
	60	10	8,8	11	9	9,2	10	58

Courses I expect to attend in the next year:

- FUNCTIONAL ANALYSIS
- DYNAMICAL SYSTEMS BASICS
- CONTROL SYSTEMS
- ENGLISH

Next years

3-D model for evaluating the thermal fatigue of the plasma facing components (PFCs) -----> ENEA (BRASIMONE)

Tokamak material structures thermo-mechanical stress analysis

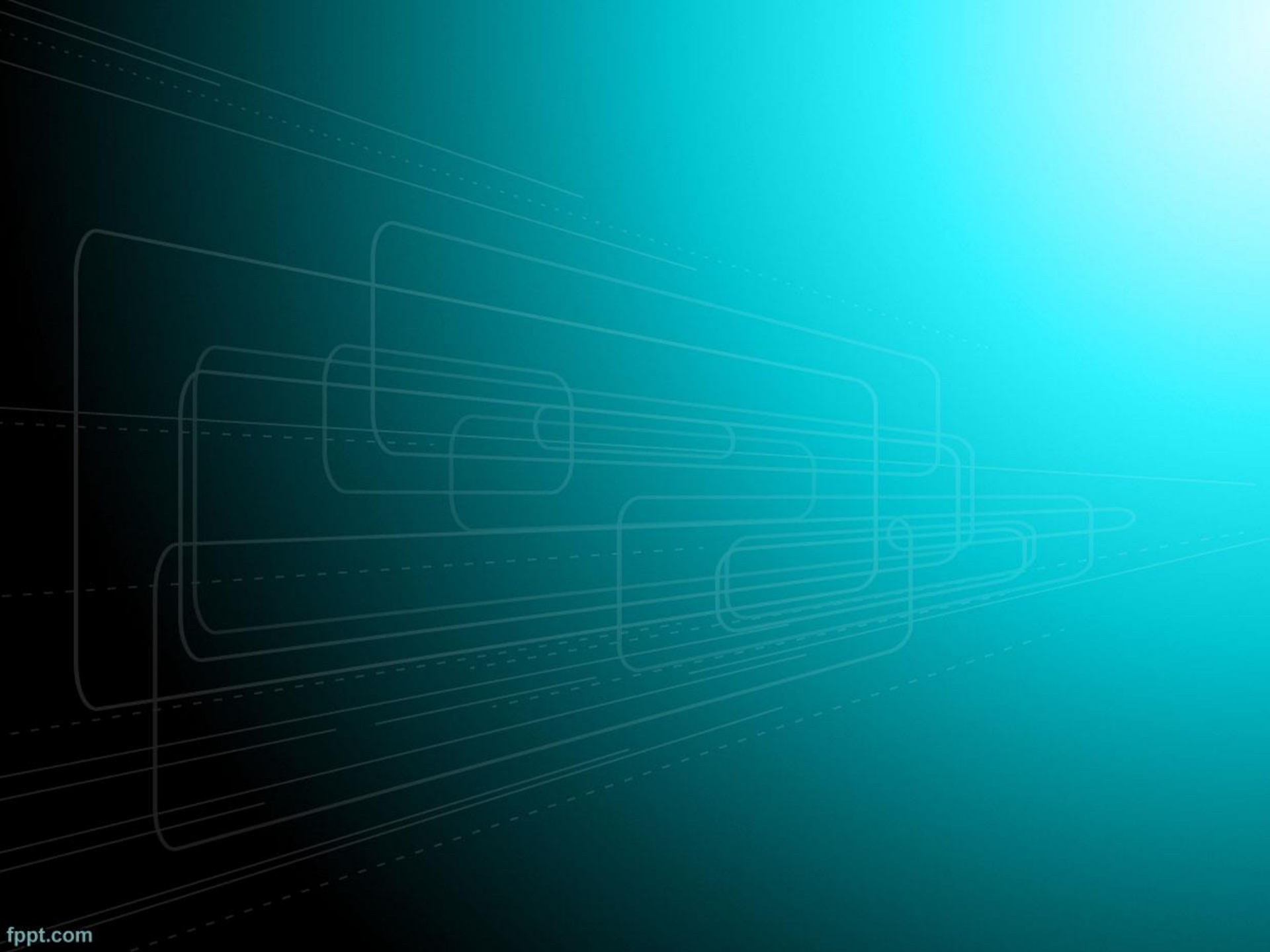
Detachment feasibility evaluation and closed loop control design

Plasma external conductors position optimization for next generation reactors

Comparisons between sweeping and other heat load spreading techniques

The background features a teal-to-cyan gradient. Overlaid on this are several white, thin, overlapping rectangular outlines that create a sense of depth and perspective, as if they are receding into the distance. Some lines are solid, while others are dashed, adding to the abstract, architectural feel of the design.

Thanks for your attention!

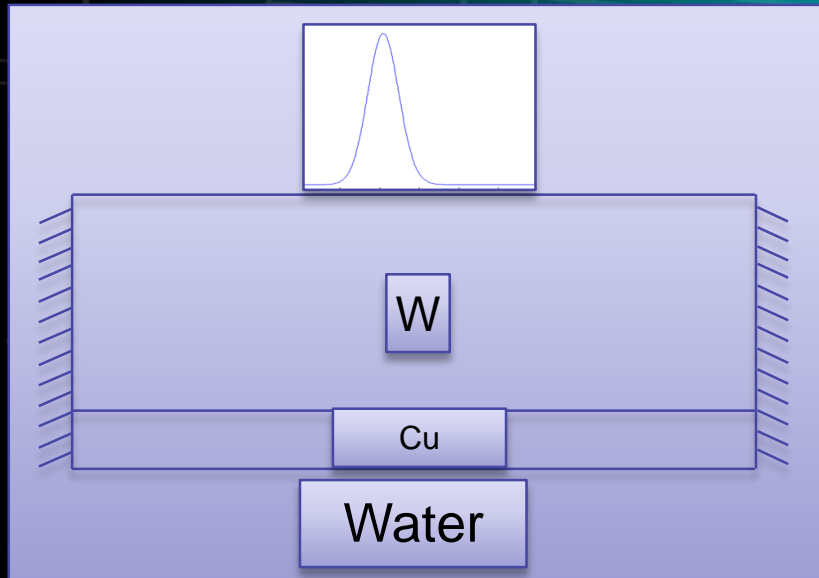


My research activity

%Methodology:

2-D FEM model implementation (my main contribution)

$$\nabla \cdot (k\nabla T) = \rho c \frac{\partial T}{\partial \theta}$$



$T_W(x, y, 0) = T_{Cu}(x, y, 0) = 200^\circ\text{C}$	$0 \leq x \leq L_x, 0 \leq y \leq L_y$
$-k_{Cu} \frac{\partial T(0, y, \theta)}{\partial x} = 0$	$0 \leq y \leq L_{y,Cu}, \theta > 0$
$-k_{Cu} \frac{\partial T(L_x, y, \theta)}{\partial x} = 0$	$0 \leq y \leq L_{y,Cu}, \theta > 0$
$-k_{Cu} \frac{\partial T(x, 0, \theta)}{\partial y}$ $= \bar{h}_{c,eff}(T_{Cu,lower} - T_{water})$	$0 \leq x \leq L_x, \theta > 0$
$-k_{Cu} \frac{\partial T(x, L_{y,Cu}, \theta)}{\partial y}$ $= -k_W \frac{\partial T(x, L_{y,Cu}, \theta)}{\partial y}$	$0 \leq x \leq L_x, \theta > 0$
$-k_W \frac{\partial T(0, y, \theta)}{\partial x} = 0$	$L_{y,Cu} \leq y \leq L_{y,W}, \theta > 0$
$-k_W \frac{\partial T(L_x, y, \theta)}{\partial x} = 0$	$L_{y,Cu} \leq y \leq L_{y,W}, \theta > 0$
$-k \frac{\partial T(x, L_{y,W}, \theta)}{\partial y} = \dot{q}$	$0 \leq x \leq L_x, \theta > 0$